



2<sup>nd</sup> SCIENTIFIC WORKSHOP

May 20–23, 2013

ADVANCED TECHNOLOGIES OF ELECTROMAGNETIC  
FIELD ASSISTED CONSOLIDATION OF MATERIALS

Key Laboratory for Electromagnetic Field Assisted  
Processing of Novel Materials

# Multiscale modeling of Spark Plasma Sintering via COMSOL™ Multiphysics

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# Outline

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1. The scheme of the SPS multiscale modeling approach

2. Micro scale temperature distribution in the powder particle

3. Modeling SPS as a hot-pressing

4. Free sintering by COMSOL™

5. Future development

# Multiscale modeling of SPS

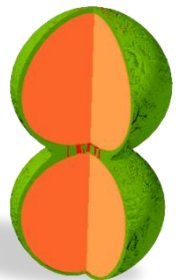
## Inter contact softening hypothesis.

**Problem 1**  
Estimation of the micro inhomogeneity of the temperature distribution

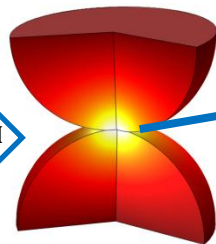
Stationary  
Temperature  
Field

**Problem 2**  
Macroscopic modeling  
of the specimen  
shrinkage kinetics  
during SPS

*Metal Powder particles with  
oxide layer in contact area*



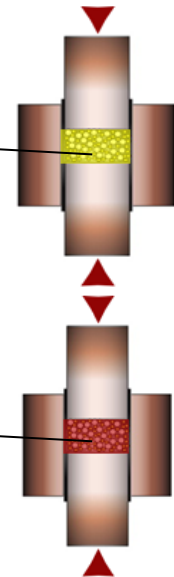
COMSOL™



*LOCAL  
TEMPERATURE*

$T_{\text{local contact}}$

$T_{\text{homogenized}}$

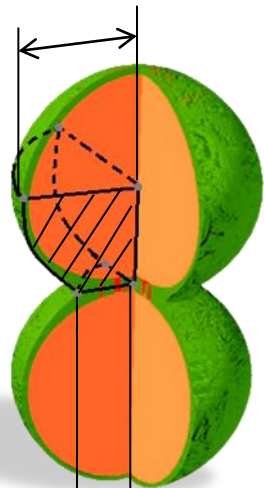


# Estimation of the micro inhomogeneity of the temperature distribution

## CONTACT of the COPPER PARTICLES

With OXIDE layer

Radius =  $2 \div 200 \mu\text{m}$



Contact Area Radius =  $\text{Radius}/5$

## Equations:

- Heat Transfer equation
- Electric Field equation

## Boundary conditions:

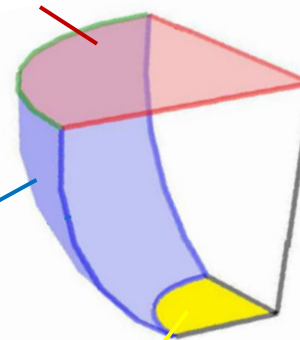
$$T_0 = 1000 \text{ K}$$

$$\vec{n} \Delta \vec{J}_{\text{oxide-metal}} = \frac{\sigma_{\text{oxide}}}{d_{\text{oxide}}} \Delta U_{\text{oxide-metal}}$$

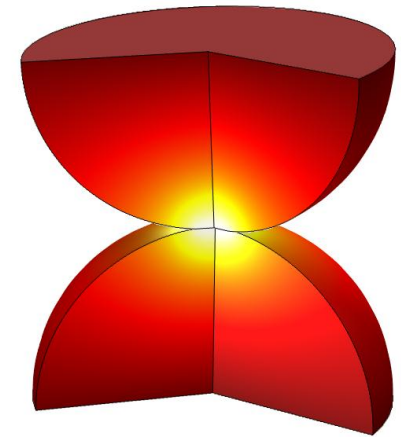
$$\Delta U_{\text{oxide-metal}} = 0,001 - 0,04 \text{ V}$$

- Current Insulation
- Thermal Insulation

$$V = 0 \text{ V}$$



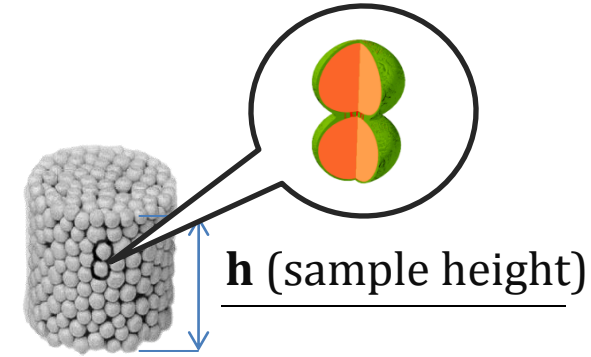
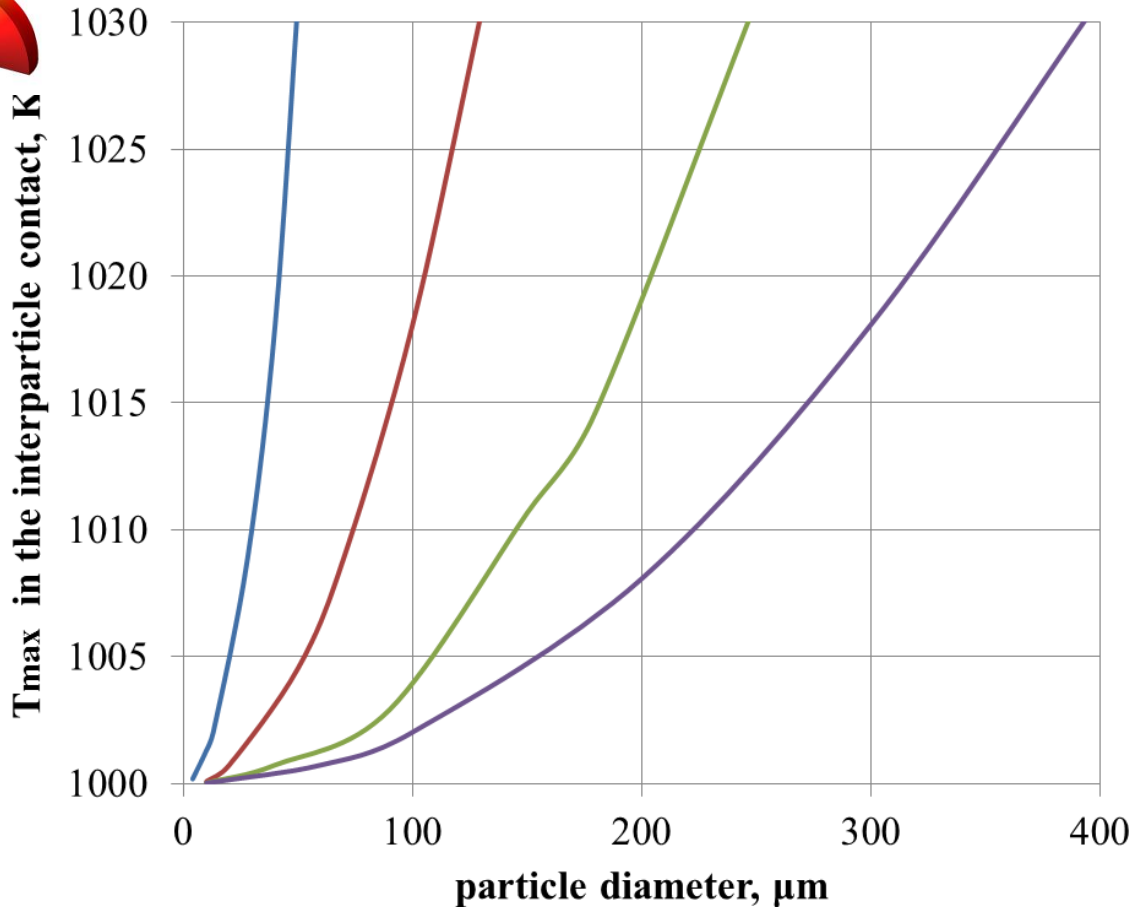
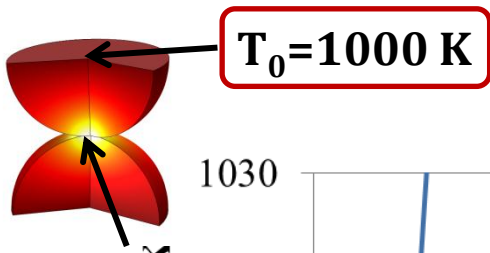
COMSOL MULTIPHYSICS®  
Capture the Concept™



**stationary LOCAL TEMPERATURE DISTRIBUTION**

# Micro-Scale Modeling results:

## Maximum temperature in contact area with presence of an oxide layer



- T, K:
- $h=0.002 \text{ m}$
  - $h=0.005 \text{ m}$
  - $h=0.01 \text{ m}$
  - $h=0.015 \text{ m}$

# Modeling SPS as a hot-pressing (based on microscopic temperature distribution)

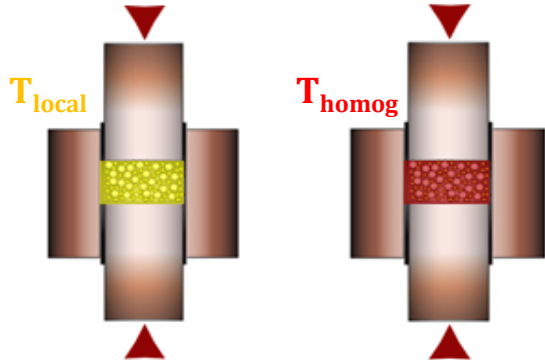
$$\sigma_{ij} = W^{m-1}(\theta) \cdot A_1 \cdot \left( \exp\left(-\frac{Q_c}{RT}\right) \right)^{-m} \left[ \frac{\sigma(\theta)}{\dot{\epsilon}} + \left( \frac{\sigma(\theta)}{\dot{\epsilon}} - \frac{1}{\sigma(\theta)} \right) \dot{\epsilon} \right] \quad [1] \text{ E.A. Olevsky, M. Sci. En., 1998}$$

**Copper particle diameter:**

$$d = 100 \mu\text{m}$$

**Applied Stress:**

$$\sigma_z = 30 \text{ MPa}$$

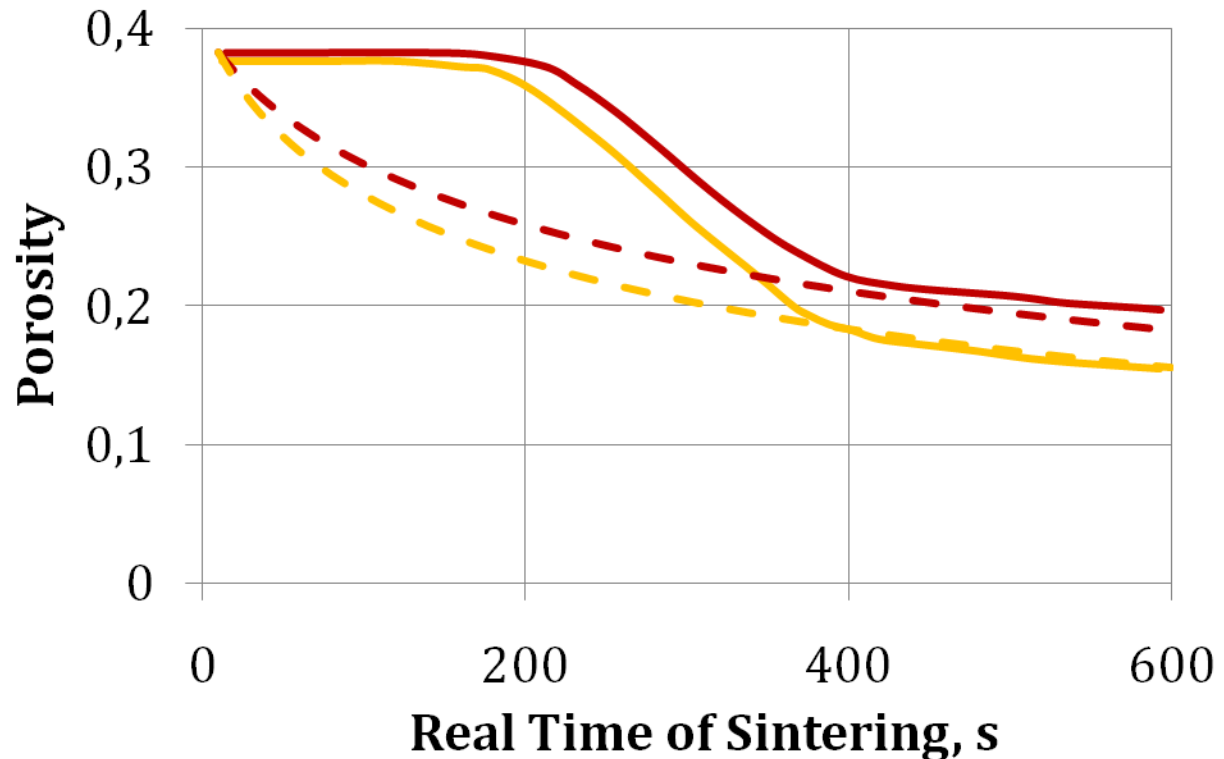
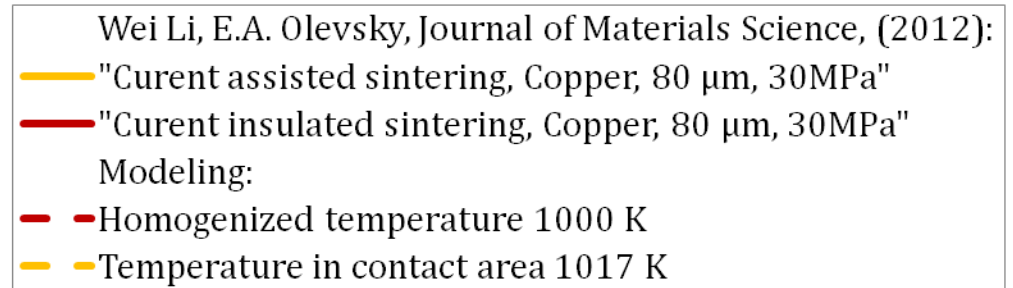


**Power-law parameters:**

$$A_1 = 1,19 \times 10^6 \left[ \frac{\text{kg} \times \text{s}^{\text{m}-2}}{\text{m}^{\text{m}+1}} \right]$$

$$m = 0,34$$

$$Q_c = 197 \text{ kJ / mole}$$



# Free Sintering in COMSOL™

- Continuum Theory of Sintering

$$2\eta_0 \left[ \dot{\varphi} \varepsilon_{ij} + \left( \psi - \frac{1}{3} \varphi \right) \dot{\varepsilon} \delta_{ij} \right] + P_L \delta_{ij} = 0$$

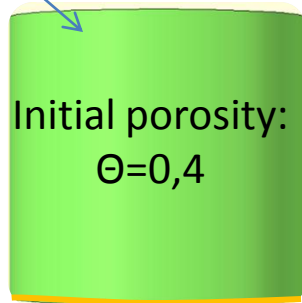
Sintering Stress

- Porosity kinetics

$$\frac{\partial \theta}{\partial t} - \nabla_i [(1 - \theta) \dot{u}_i] = 0$$

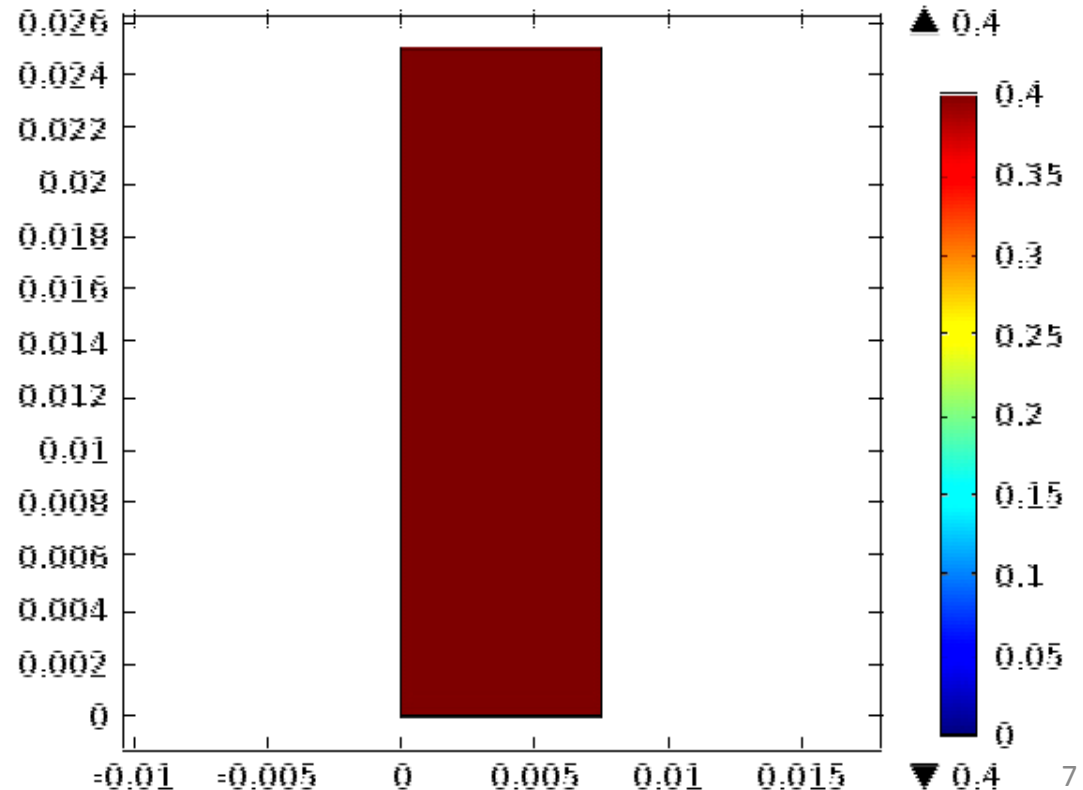
[1] E.A. Olevsky, M. Sci. En., 1998

Body load:  
Sintering Stress  $P_L$



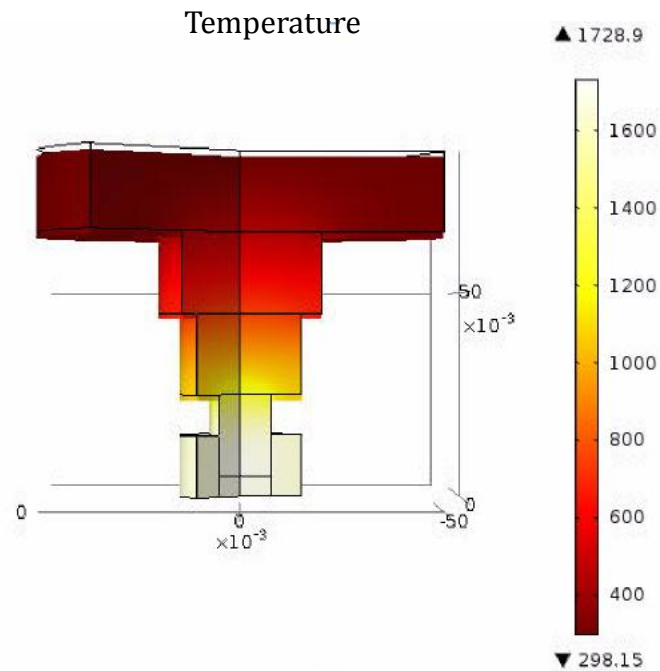
Prescribed displacement:  
 $U_z = 0$

Time=0 Surface: Porosity Kinetics (1)



# Future Development

Building of the multiscale **electro-thermo mechanical** model of SPS of the **non-linear viscous** body in COMSOL™ Mutiphysics with full tooling.



**Thank you for your attention!**